

NATURAL BITUMEN SELENIZZA APPROPRIATE CHOICE FOR HIGH PERFORMING ASPHALT MIXES

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Introduction



The mine of **Selenice** is located in southeast **Albania**.

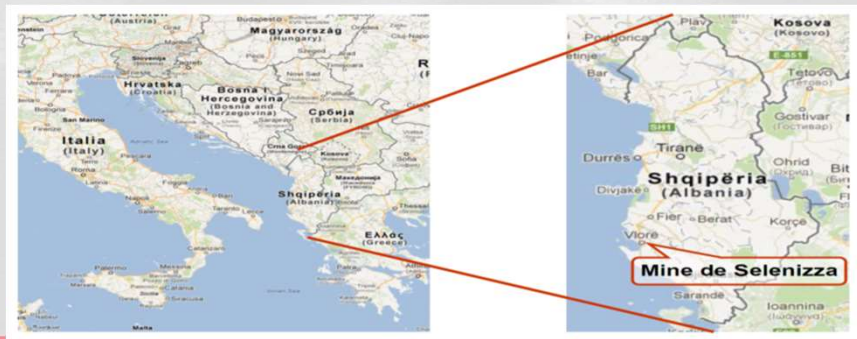
It has been mentioned since ancient times **by Aristotle &** actively exploited by **the Romans**.

in **1868**, The French **geologist Coquand** published a **geological description**

The **ottoman government** transferred rights to the **French (1871), Italians (1919-1943)**.

After the World War II exploited by the **Albanian** government.

Since 2001, the mine is managed by the **French company KLP Industries**



Natural Asphalts : modifiers of road bitumen



- **Thermo-rheological characterization**

Study was carried out by the University of Rome "**LA SAPIENZA**"

Three natural asphalts :

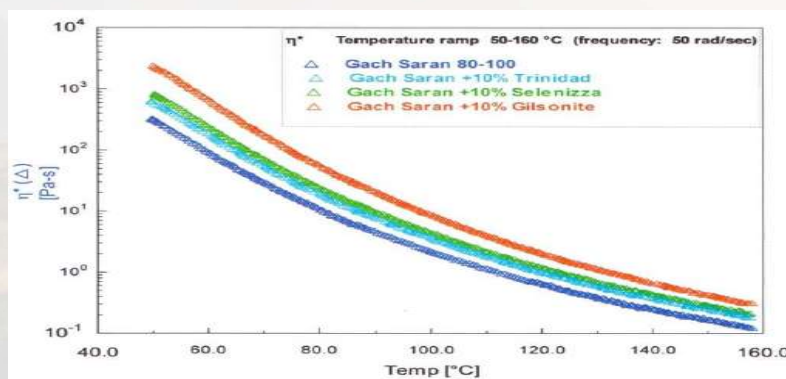
***Straight Run bitumen*, penetration grade 80/100 + 10 % natural asphalt**

Natural asphalt	Bitumen content (%)	Asphaltènes content(%)	Penetration (à 25°C,1/10 mm)	R&B (°C)
Gilsonite	> 99	70	0	160-170
Selenizza	85-90	42*	0	115
Trinidad	53-55	33-37	1 - 4	93-98

Dynamic rheological analysis



- Medium and high temperatures (50 – 160°C), depends exclusively on the asphaltene content

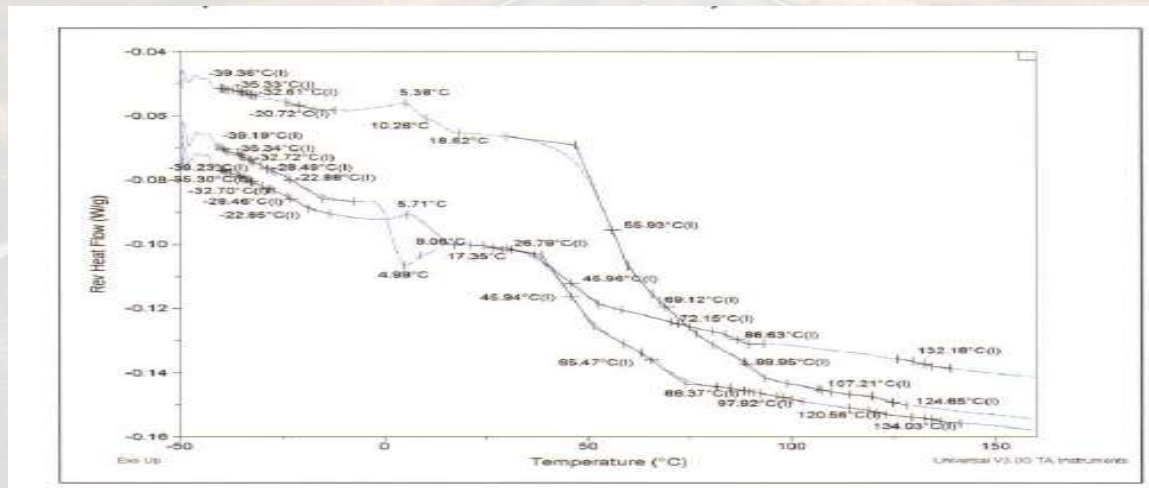


- **Viscosity values increase, the viscosity curves shift upwards**
- **Modifiers don't affect the internal interactions between the asphaltene components**
- **Compatible additives**

Modulated Differential Scanning calorimetry MDSC:



- **Reversing curve** is more indicative for **vitreous transitions**
- **Trinidad & Selenizza** : affect the **lower limit** of the softening range of the straight run bitumen (+55,8 °C → 45,9°C), hence **dilution effect**
- **Gilsonite**, only expands the softening range to **higher temperatures**
- **Increase of consistency, viscosity and stability** of base bitumen



Characteristics of natural bitumen Selenizza



• *Physic-chemical properties*

- organic phase **similar** to petroleum bitumen, **higher content** of polar fractions
- **vitreous transition** at **higher temperatures**, colloidal instability sol or sol-gel
- addition of natural bitumen **does not affect** the glass transition of bitumen
- 35/50 compared to modified alternative → $T_g = -23.1^\circ\text{C}$ versus $T_g = -19.3^\circ\text{C}$
- better resistance of natural bitumen to **brittle fracture**

IATROSCAN fractions

SARA IATROSCAN method		Saturated [%]	Aromatic [%]	Resin [%]	Asphaltene -i [%]	I_c
Purified sample- depth	Average	1,7	24,8	35,1	38,4	0,67
	Standard deviation	0,35	2,29	1,35	1,88	
Purified sample- surface	Average	1,5	22,7	37,2	38,6	0,67
	Standard deviation	0,14	1,37	1,90	1,58	
Raw sample- depth	Average	1,6	23,8	34,6	40,01	0,71
	Standard deviation	0,29	1,40	1,16	1,99	
Raw sample- surface	Average	1,6	19,7	37,9	40,8	0,73
	Standard deviation	0,24	2,02	1,60	2,74	

Complex Modulus

<u>Complex modulus</u>	Measures at 100°C, 5 Hz	
	$ E^* $ [GPa]	δ [°C]
Albanian Natural Bitumen	0,95 - 1,27	48,3 - 51,7

Evolution of Glass transition temperatures

	Total heat flux				
	T_{g1} [°C]	T_{g2} [°C]	T_{g2} [°C]	ΔT_{g1} [°C]	$\Delta\Phi$ [W/g]
Petroleum bitumen 50/70	-31,9	-22,9	-13,2	18,6	0,022
Mixed with 5% SLN	-30,9	-23,1	-13,8	17,1	0,019
Mixed with 10% SLN	-30,3	-23,1	-13,3	17,0	0,018
Mixed with 15% SLN	-32,1	-23,3	-13,4	18,8	0,019
Natural asphaltite SLN	-12,6	-1,1	16,2	28,8	0,021

Aging retarder

50/70 road bitumen + 5%, 10% & 15 % Selenizza

versus

equivalent bitumen 35/50, 20/30 & 10/20

RTFOT tests (manufacturing) & PAV (in-service aging)

Aging effect was quantified using mathematical expression:

$$EV_x = \frac{|x^{RTFOT+PAV} - x^{New}|}{x^{New}} * 100$$

EV_x: the evolution of mechanical property X

1. Changes of modified specimen, lower than those of 50/70.

2. Changes are attenuated with the increase of the % SLN

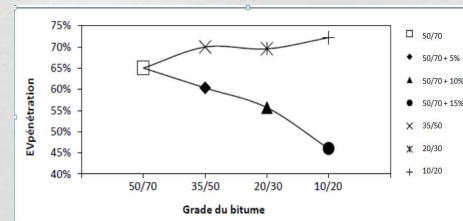
3. Modified bitumen vs equivalent road bitumen

are characterized by minor changes

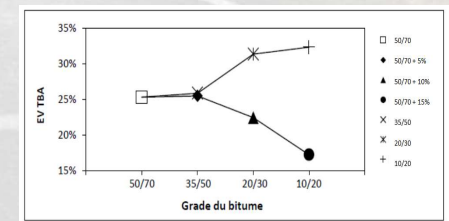
G* and phase angles show same trend in changes.

Description	Penetration (dmm)					TR&B (°C)				
	New binder	After RTFOT	Δ ₁ (%)	After PAV	Δ ₂ (%)	New binder	After RTFOT	Δ ₁ (%)	After PAV	Δ ₂ (%)
Petroleum 50/70	54	37	31.5	19	64.8	49	53.4	8.9	61.4	25.3
Mixed with 5%	38	27	28.9	15	60.5	52.6	57.2	8.7	66.0	25.4
Mixed with 10%	28	21	25	13	53.5	56.2	60.8	8.1	68.8	22.4
Mixed with 15%	20	14	30	11	45	61.6	65.4	6.1	72.2	17.2
Petroleum 35/50	40	27	32.5	12	70	52.6	56.8	7.9	66.2	25.8
Petroleum 20/30	23	12	47.8	7	69.5	60.0	67.0	11.6	78.8	31.3
Petroleum 10/20	18	9	50	5	72.2	65.0	72.6	11.7	86.0	32.3

Evolution of penetration



Evolution of R&B



Highway implementation examples



HMA in Switzerland

High-level of traffic constraints & Very harsh climatic conditions (-20°C to + 40 °C)
→ *incorporated in national standard the HMA concept*

- HMA class 1 for improving rutting resistance
- HMA class 2 for improving rutting & fatigue resistance

2 alternatives of mix design was tested:

3.9% Shell Cariphalte 25 RC+ **1.4% SLN** = **5.3%** (Selenizza **26%** of the total binder)

3.9% Shell Cariphalte 25 RC+ **1.6% SLN** = **5.5%** (Selenizza **29%** of the total binder)

Modulus and Fatigue tests results **clearly exceed** the Swiss HMA specifications (14 000 MPa and 135 μ def).

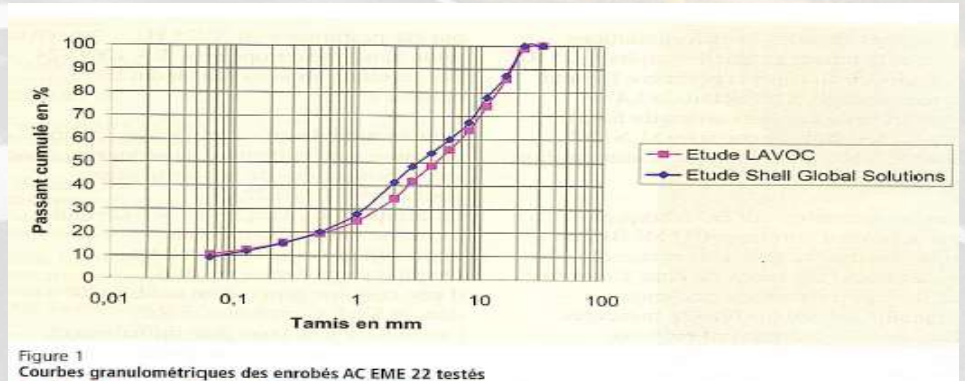
To prevent the **cracking risk** at low temp., **final job** mix formula: **4.7% Shell PmB + 1.4% SLN = 6.1%**

Modified binder → **10/20** paving grade bitumen: **penetration = 13 [0.1 mm]** and **TR&B = 86,7 [°C]**

Bonder composition	Unity	Mix design 1	Mix design 2
Shell Cariphalte 25 RC	%	3,9	3,9
Selenizza SLN	%	1,4	1,6
Theoretical binder content (% by mix mass)	%	5,3	5,5
Complex modulus at 15°C/10Hz (EN 12697-26)	MPa	19 441	18 336
Fatigue resistance at 10°C/25Hz (EN 12697-24)	μ def	139	145

ϵ_6 (extrapolated) \approx **150 μ def**

Modulus (15°C/10 Hz) = 15 100 MPa





Highway A8 “Olimpia Odos” (Greece)



375 km highway network designed according to **French Standards** applied to **Greek reality and experience**

Road structure → **DBM** (Dense Bitumen Macadam) **base course**

Anti-rutting **binder course AC (5 cm)**

Anti-skid **TAC** (thin asphalt concrete) **wearing course (2.5 cm).**

Base & Binder Courses → tested different kind of binders:

- bitumen **50/70**
- bitumen **50/70 + 8% Selenizza**
- bitumen **30/50**
- **PR PLAST** modified bitumen

STIFFNESS MODULUS (Indirect Tensile Test)

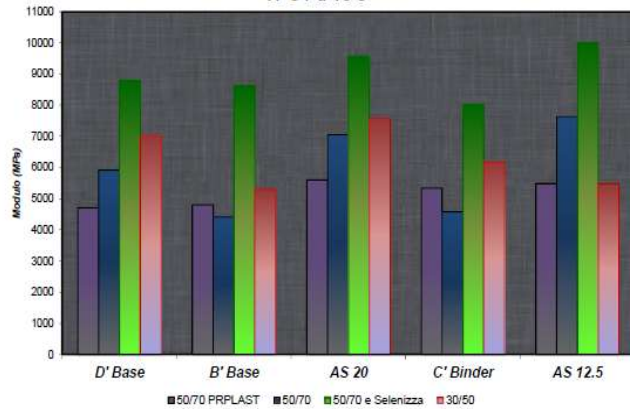
STIFFNESS MODULUS (Two Point Bending Test)



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LABORATORY TEST RESULTS
STIFFNESS MODULUS

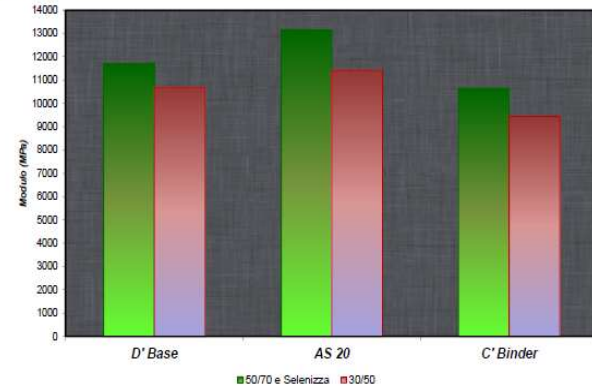
IT-CY a 18°C



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LABORATORY TEST RESULTS
STIFFNESS MODULUS

2PB-TR a 15°C



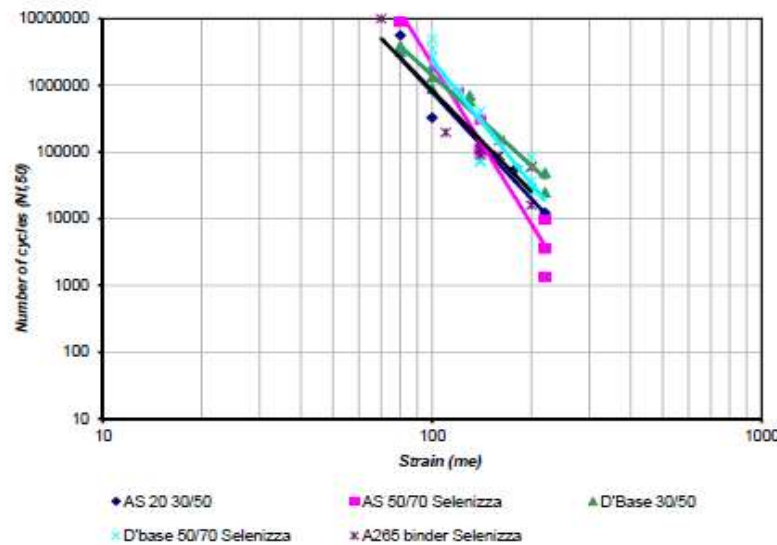


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LABORATORY TEST RESULT FATIGUE RESISTANCE 2PB-TR



SUMMARY OF FATIGUE TESTS 2PB-TR, 10°C, 25 Hz



Material	Bituminous binder	Fatigue ϵ_6 10 °C, 25 Hz	Class asphalt mix
STS A265 B' binder course	50/70 + 8% Selenice Pen = 39	101.6	DBM4
STS A 260 D' base course	30/50 Pene = 45	108	DBM3
STS A 260 D' base course	50/70 + 8% Selenizza Pen=39	112	DBM4
AS 20 base course	50/70 + 8% Selenizza Pen = 39	110	DBM4
AS 20 base course	30/50 Pen= 45	95	DBM3

	TAC	AC	DBM2	DBM3	DBM4	HDM
10°C	7200	7200	12 300	12 300	14 550	17 000
18°C	4320	4320	7500	7500	8870	12200
ϵ_6	-	-	80	90	100	130
-1/b	-	-	5	5	5	5
SN	-	-	0,3	0,3	0,3	0,25
ν	0,35	0,35	0,35	0,35	0,35	0,35
Kc	-	-	1,3	1,3	1,3	1

Binder **50/70 + 8% Selenizza** higher **Stiffness and Fatigue performance** → Asphalt Mix belongs to higher project category **DBM 4**, making possible to reduce the road package **thickness** by at least **4 cm**.

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First Macedonian Road Congress / November 7-8, 2019 Skopje.

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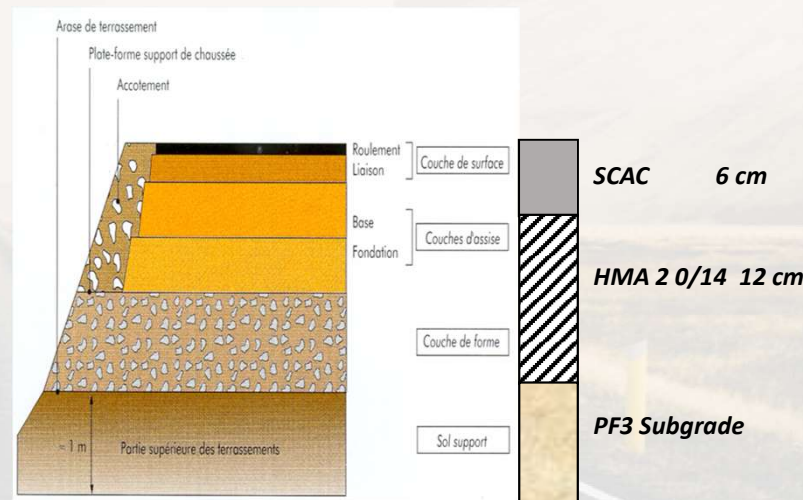
Highway A 150 (FRANCE)



PROJECT DESCRIPTION

17,5 km new roadway in **A 150 Highway**

technical specifications according to the CE standard NF EN 13108-1, was implemented base course **EB 14 ASSISE 20/30**

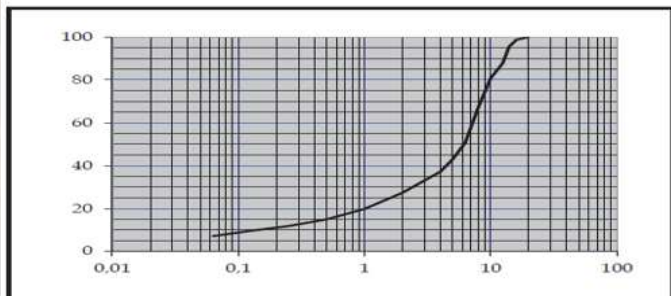


Two types of binders were analyzed:

- *The basic HMA mix design: 30% RAP+ 20/30 penetration grade bitumen*
- *Alternative studied: 30% RAP + 50/70 grade bitumen + 1,5 % Selenizza SLN*

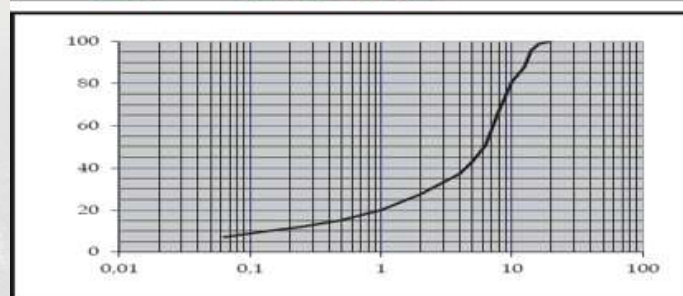
HMA 0/14 → 20/30 + 30% RAP

FORMULE			
19,5%	0/5	STEMA	
21,8%	5/8	STEMA	
12,3%	8/11	STEMA	
11,4%	11/16	STEMA	
1,4%	FILLER CONS		
29,9%	AE		
	apport liant AE	avec	5,0 %TL
3,7%	20/30		
5,2%	BITUME TOTAL		



HMA 0/14 → 50/70 + 30% RAP + Selenizza

FORMULE			
20,4%	0/5	STEMA	
21,8%	5/8	STEMA	
12,3%	8/11	STEMA	
11,4%	11/16	STEMA	
0,3%	SLN 120	FILLER	
1,4%	FILLER CONS		
29,9%	AE		
	apport liant AE	avec	5,0 %TL
2,5%	50/70		
1,50%	SLN 120		
5,2%	BITUME TOTAL		



Same composition of materials, grading curve and % of binder

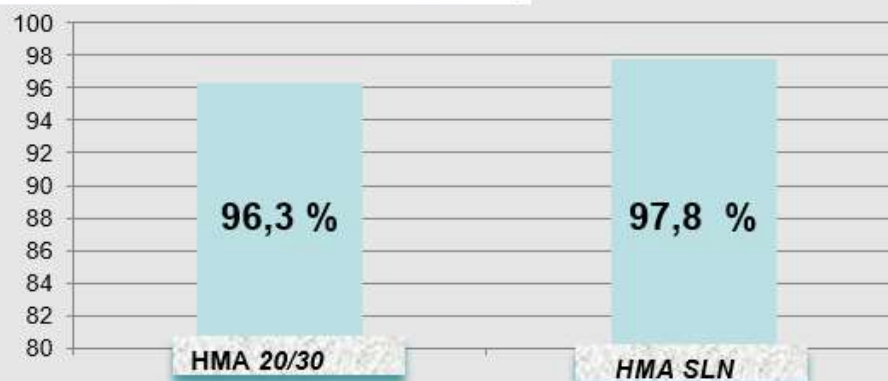
Water sensitivity

HMA 20/30

Sensibilité à l'Eau EN 12697-12 Méthode B			
COMPACTITE	94,9%	ESSAIS MECANIQUES	
INDICE VIDES	5,1%	C _D à 18° kPa	17918
MVRG t/m ³	2,767	C _W à 18° kPa	17250
MVR t/m ³ *	2,545	i/C (%)	96,3
MVA t/m ³	2,416	K	3,45

HMA SLN

Sensibilité à l'Eau EN 12697-12 Méthode B			
COMPACTITE	95,1%	ESSAIS MECANIQUES	
INDICE VIDES	4,9%	C _D à 18° kPa	20623
MVRG t/m ³	2,766	C _W à 18° kPa	20178
MVR t/m ³ *	2,544	i/C (%)	97,8
MVA t/m ³	2,418	K	3,46



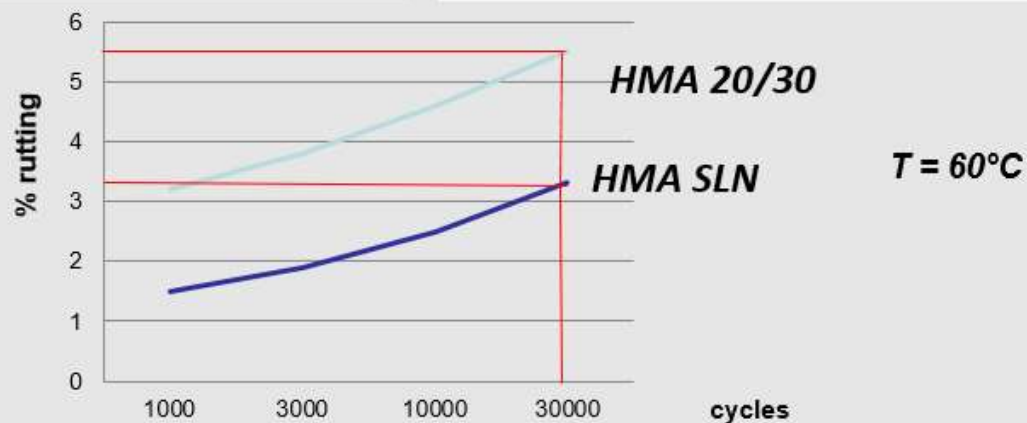
The 2 specimen were compacted at the same void percentage 5%



Resistance to rutting

ESSAI D'ORNIERAGE EN 12697-22		
% de vides des éprouvettes		4,9 %
N Cycles	% ornière moyen	Specific.
1 000	3,2%	
3 000	3,8%	
10 000	4,6%	
30 000	5,5%	< 7,5%

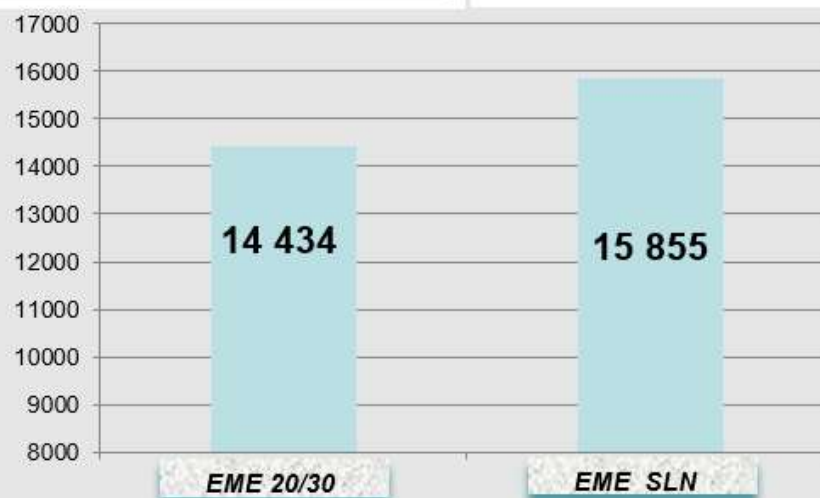
ESSAI D'ORNIERAGE EN 12697-22		
% de vides des éprouvettes		4,7 %
N Cycles	% ornière moyen	Specific.
1 000	1,5%	
3 000	1,9%	
10 000	2,5%	
30 000	3,3%	< 7,5%



Elastic modulus

<i>TRACTION INDIRECTE EN 12697-26 Annexe C</i>	
% de vides	5,1
Module 15°C, 124ms (MPa)	14434

<i>TRACTION INDIRECTE EN 12697-26 Annexe C</i>	
% de vides	5,0
Module 15°C, 124ms (MPa)	15855



T = 15°C

Fatigue

HMA 20/30

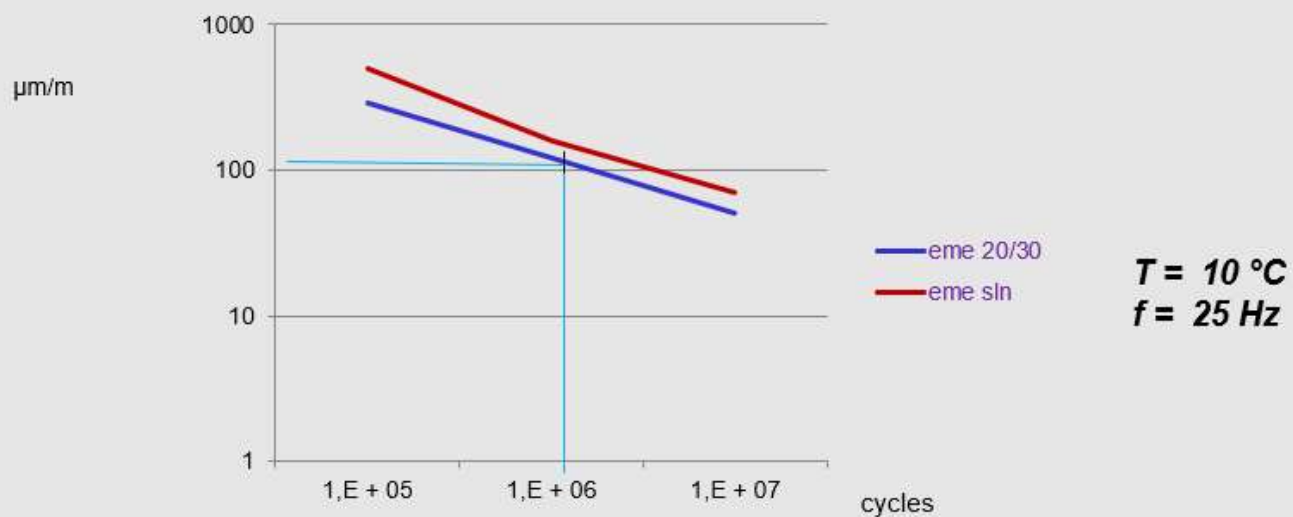
ESSAI DE FATIGUE EN 12697-24 Annexe D

MVA (t/m³) : 5 % de vides
Déformation relative à 10°, 25Hz : 134,1 µm/m

HMA SLN

ESSAI DE FATIGUE EN 12697-24 Annexe D

MVA (t/m³) : 5,1 % de vides
Déformation relative à 10°, 25Hz : 137,3 µm/m





The study results **validated the** approach which consists in manufacturing the recycled HMA using a straight run bitumen **50/70 + 1,5 % Selenizza**.

LIFE CYCLE ASSESSMENT



SELENIZZA vs petroleum bitumen

Need for **bituminous binders** that meet **Life Cycle Assessment constraints**, **quantifying** the **environmental impact** of construction materials and comparing **potential solutions** based on **scientific data**

Life Cycle Assessment (LCA) assess the **durability** of different materials evaluating the **environmental impact** during all the **stages of the product's life cycle**, from **cradle to grave**

University of Rome in cooperation with the company **Selenice Bitumi**, carried out a **research project**, to **analyze and compare** for the first time, in terms of **energy consumption** and **CO₂ emission** between:

1. the various steps necessary to produce the **conventional bitumen from crude oil**
2. the production process of the **Albanian natural asphalt** (Selenizza)

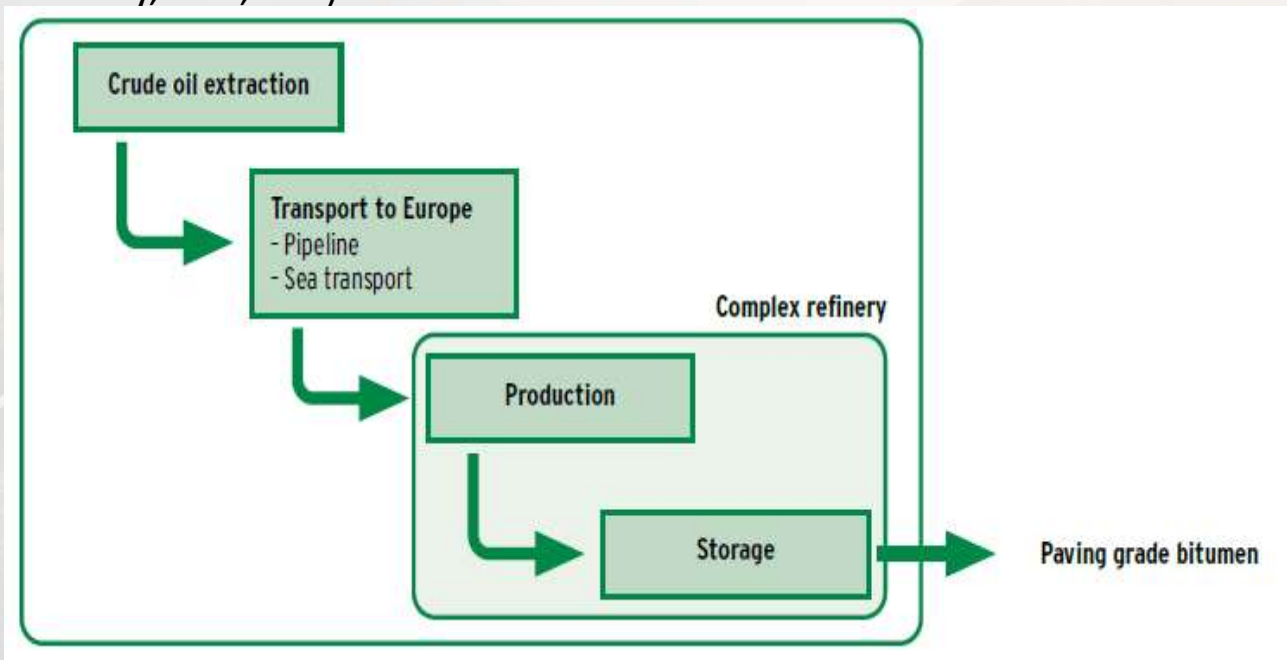


Petroleum bitumen production chain (cradle to grave approach)

Guidelines of EU regulations (ISO 1440 and 14044) for **environmental assessment, LCA and LCI.**

Data made available from **relevant bodies** and specialized **agencies** such as **Eurobitume & EAPA**

The **Life Cycle Inventory (LCI)** for **straight-run bitumen**, has evaluated all the **resources & inputs** (raw materials, electricity, fuel, etc.)



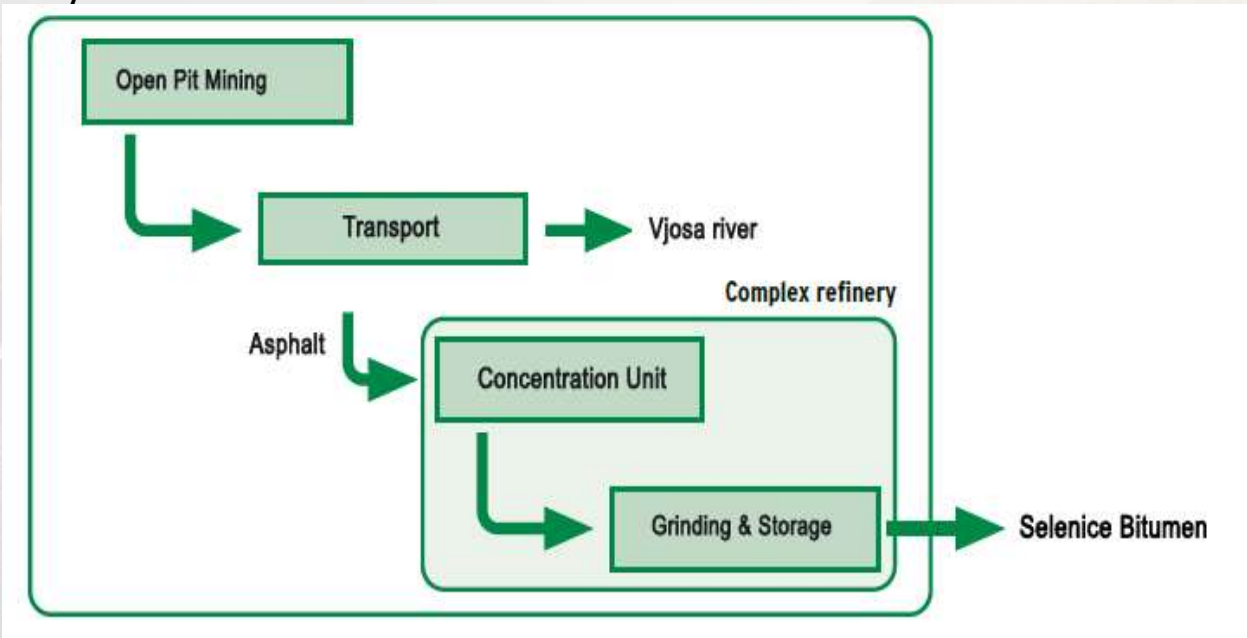
Deposit of natural bitumen Selenizza



The production chain of natural bitumen Selenizza

The production process is **far simpler** with a direct impact on the **energy saving**; also the **transport cost is reduced** to minimum because the **processing unit is located close to the deposit**

Selenice manufactures on site: 1. **Raw ore** (natural bitumen) 2. **The fuel** (bituminous coal) used for refining ore in furnaces 3. **The residual inorganic materials**, transported and **deposited** close to a **river** in the vicinity



Comparison of results

Bitumes routiers de distillation						
Total	Consommation d'énergie	MJ/t				4,71
CO ₂	Emissions dans l'air	g	144563	37422	7831	226167
L'asphalte naturel Selenizza						
Total	Consommation d'énergie	MJ/t				2,376
CO ₂	Emissions dans l'air	g	59300	4500	59145	127298

- **Selenizza's** production cycle has an **environmental impact** approximately **44% less** than the distillation bitumen
- **Energy consumption** is also reduced by **around 50%** compared to bitumen produced from crude oil

CONCLUSIONS

- **100% compatible** with petroleum bitumen & PmB
- **High Permanent Deformation Performance HMA**
- Improved **adhesion of bitumen on the aggregates**
- Reduction in Pavement **thickness**
- Better **workability of asphalt**
- **Aging retarder & long-life** flexible pavements for heavy traffic
- **Environmentally friendly** bitumen



Thank you for your attention