



# **Contribution of natural asphalts to the implementation of EME mix for cold climate**

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# Outlines

- 1. *Modification of petroleum road bitumen by the addition of natural asphalts***
- 2. *Characteristics and low temperature behaviour of SelenizzaSLN and natural asphalt modified binders***
- 2. *Mix design examples used in countries with vast temperature fluctuations. Selection criteria***
- 4. *Natural bitumen: An environmentally friendly product***
- 5. *Conclusions***



# ***Modification of road bitumen by natural asphalts***

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*Toward High Performance Asphalt Concrete (HPAC) for Cold Climates  
Montreal, September 30, 2016*

# Characterisation of different natural asphalts

- A study was carried out by the University of Rome “**LA SAPIENZA**” to characterize **natural bitumen** and evaluate their **contribution** to the modification of **straight-run bitumen**
  - The aim of this research work was to **characterize** some of the natural asphalts, most diffused commercially and to evaluate their **efficiency as modifiers**
- **Three natural asphalts** were selected:

Natural asphalt	Bitumen content (%)	Asphaltènes content(%)	Penetration (à 25°C,1/10 mm)	R&B (°C)
Gilsonite	> 99	70	0	160–170
Selenizza	85-90	42*	0	115
Trinidad	53-55	33-37	1 - 4	93–98

- An Iranian **Straight Run bitumen** (Gach Saran) with penetration **80-100**, was **added with each** of the three types of natural asphalts :
- by the percentage of **10%**
  - at a minimum temperature of **150 – 180 °C**

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# Characterisation of different natural asphalts

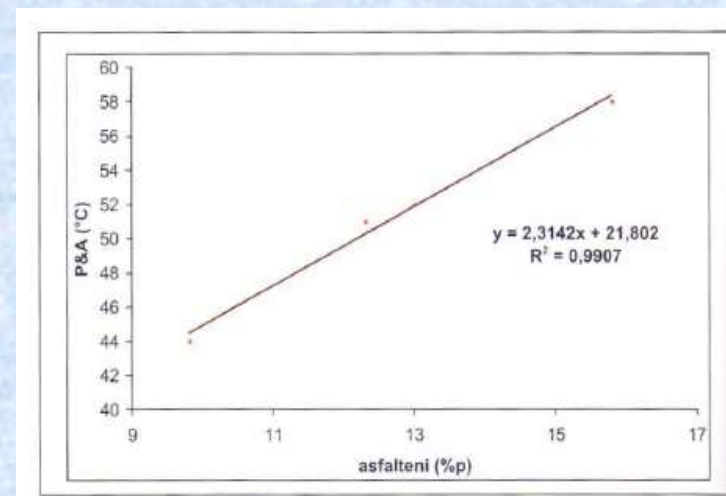
- In order to analyze the nature of the modification, two techniques have been used:
  - **Dynamic rheological analysis**
  - **Modulated Differential Scanning Calorimetry (MDSC)**
- The **rheological analysis** was carried out with a rotating rheometer under:
  - **isochronal conditions**, with temperature scanning, for the assessment of viscoelastic behavior in relatively **high temperatures**
  - **isothermal conditions**, with frequency scanning, for determining the characteristics in **low temperature range**
- The trials were performed in the respective **linear viscoelastic areas** for each sample in order to apply the temperature-frequency equivalency principle and **generate the master curves**

# Characterisation of different natural asphalts

## Effect on Penetration and Softening Point

As **expected**, for the three cases, the resulting modified bitumen was characterized by **higher softening point** (R&B temperatures) and **lower penetration values**, compared to the original standard bitumen, due to the presence of **high percentages of asphaltenes** content in the natural asphalts

Type of bitumen	Penetration at 25° (1/10 mm)	R&B Temperature °C	Asphaltene content (%)
Original bitumen	96	44	9,8
+10% Gilsonite	38	58	15,8
+10% Selenizza	67	52	13,0
+10% Trinidad	78	51	12,3



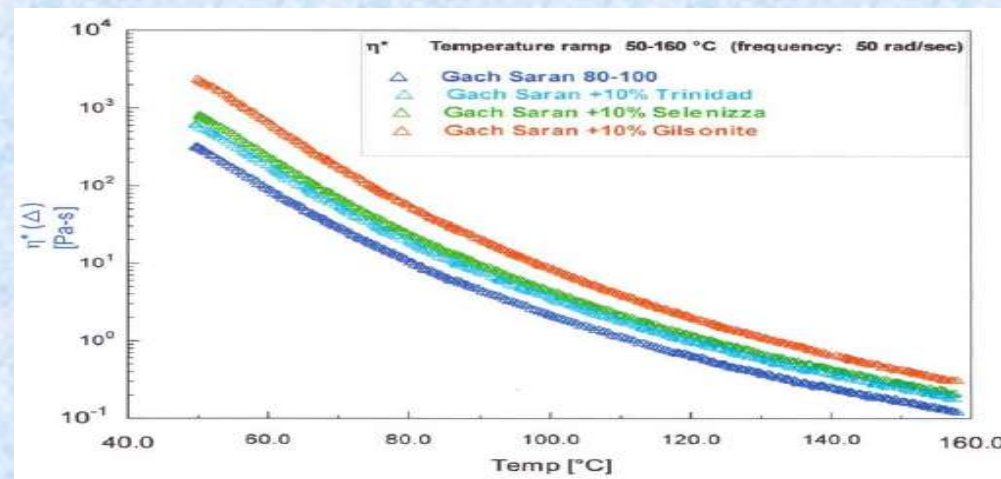
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# Characterisation of different natural asphalts

## Effect on viscoelastic properties at high temperatures

For medium and high temperatures (50 – 160°C), the rheological behavior whose softening point represent the lower limit, is not a function of the modifier quality and **depends exclusively on the asphaltenes content**



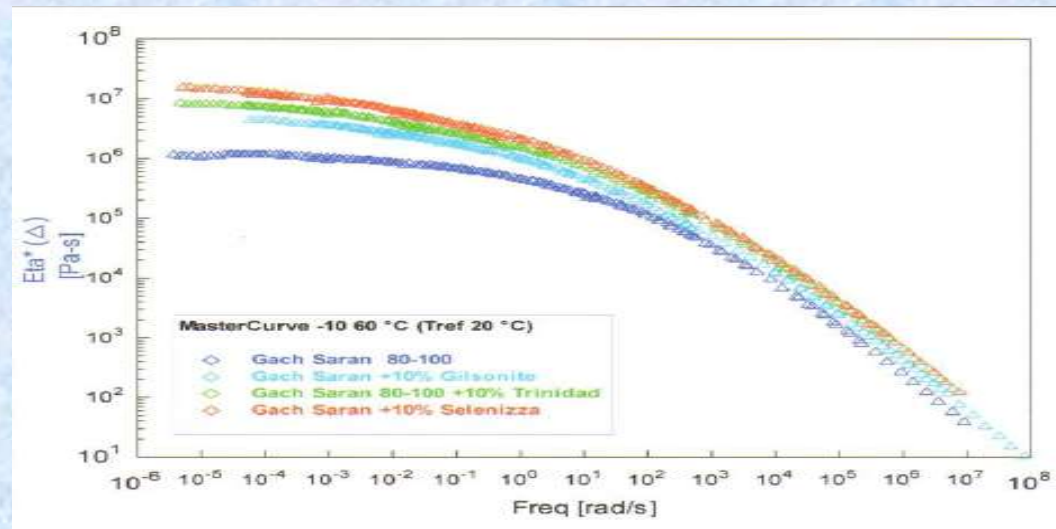
The **viscosity values increase**, the viscosity curves **shift upwards**, their shape and the slope remain unchanged and parallel for all sample types. The **modifiers don't affect the internal interactions** between the **asphaltene components** in the modified bitumen, which is a typical phenomenon for the **compatible additives**

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# Characterisation of different natural asphalts

## Effect on viscoelastic properties at low temperatures

- For the **low temperatures (10 - 60°C)**, the rheological **modifications** seem complex and are **differentiated**



- **Master curves**  $\eta^*$ ,  $G'$ ,  $G'' = f(\omega)$  drawn under reference temperatures **20°C & 60°C**. The **viscoelastic** behavior and the **ductility** of the modified samples are **impacted by the quality of the natural bitumen** (bituminous+inorganic component). At **T=20°**, inversion of the zero shear viscosity  $\eta_0$  (GS) <  $\eta_0$  (Gil) <  $\eta_0$  (Trid) <  $\eta_0$  (Sln)

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# Characterisation of different natural asphalts

## *Modulated Differential Scanning calorimetry MDSC:*

- The **samples** (7 – 10 mg), were **subjected to a modulated heating ramp** resulting from a sinusoidal temperature ripple overlaid on a linear temperature ramp:

$$dQ/dt = C_p \beta + f(T, t)$$

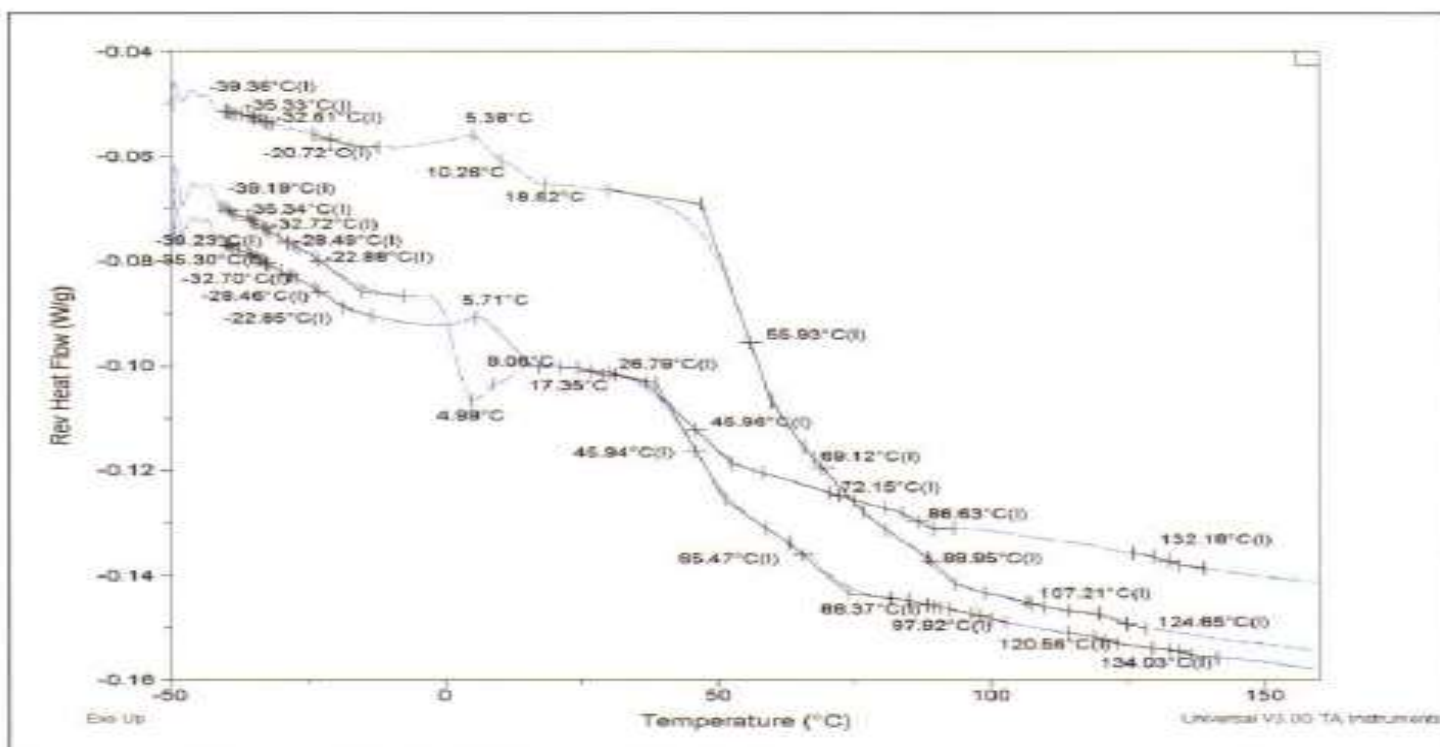
Temperature range: [ -50 °C, + 160 °C]

- For the bitumen, the **reversing curve**  $\approx 1/ C_p$  , is **more indicative**:
  - **vitreous transitions**
  - **fusions**

# Characterisation of different natural asphalts

## Modulated Differential Scanning calorimetry MDSC

Reversing curves of the mixed samples



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# Characterisation of different natural asphalts

## *Modulated Differential Scanning calorimetry MDSC:*

- The The MDSC analysis shows that the **rheological behavior** of the **petroleum bitumen** is being **modified** by the addition of natural bitumen
- **Trinidad & Selenizza** : affect the **lower limit** of the softening range of the straight run bitumen (+55,8 °C → 45,9°C) **due to the presence** of **different maltenic phases** (of lower molar mass), which **soften at lower temperatures**. The **asphaltenic phases**, result to **behave independently**. A dilution effect of the original bitumen is obtained
- **Gilsonite**, does not act as a diluent, but **expands the softening** range to **higher temperatures**
- The **modifications** operate in such a way as to **increase** the **consistency**, the **viscosity** and the **stability** of the original bitumen → natural bitumen represent **an advantageous alternative** to other additives for modifying the road pavement bitumen

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# ***Characterization of Selenizza<sup>®</sup>SLN*** | 2

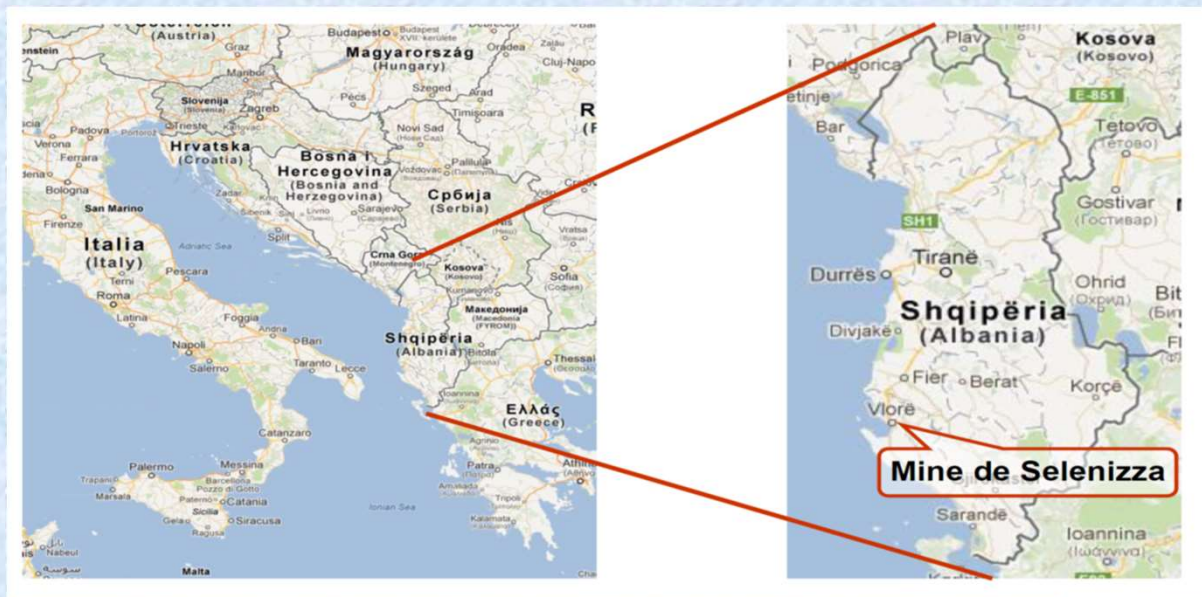
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Montreal, September 30, 2016*



# Characterisation of natural bitumen *Selenizza*®SLN

➤ The mine of **Selenice** is located in southeast **Albania**. It has been mentioned since ancient times **by Aristotle** and has been actively exploited by the Romans. After centuries of silence, in **1868**, The French **geologist Coquand** published for the first time a **geological description** of the albanian bitumen deposit. The ottoman government transferred the mine operating rights to the French (1871), followed by the **Italians** (1919-1943). After the Second World War, the mine was exploited by the Albanian government.

**Since 2001**, the mine is managed and operated by the **French company KLP Industries** and the modern bitumen production, with open pit mine operations, has witnessed a remarkable progress.



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# Principal characteristics of SelenizzaSLN

Penetration at 25°C (1/10 mm)	EN 1426	≤ 2
Softening point temperature (R&B °C)	EN 1427	≤ 120
Acidity Index (mg KOH/g)	EN 14104	3,5
Density at 20°C (g/cm <sup>3</sup> )	EN ISO 3838	1,16
Asphaltene content (% wt)	ASTM D2007-11	> 50
Mass loss at 163°C, 5 hours (%)	EN 13303	0,08



# ***Characterization of natural bitumen*** ***Selenizza®SLN***

- A **PhD thesis** was recently presented at the University of Strasbourg in France, on the **potential of using** natural bitumen in the production of **hard penetration grade binders** and **high modulus asphalt mixes** that lead to implementation of **cost effective** pavements (thin and long lasting pavement layers)
- **The study**, in line with the strategy of **sustainable industrial development**, **proposes an alternative method** using natural bitumen to produce HMA aging **resistant** and relatively **efficient at low temperatures**.
- These researches are **very topical at this time**, considering the **problems encountered** while using **hard petroleum bitumen** such as the **risk of cold cracking, rapid aging, supply difficulties**, as well as the **inability to produce hard bitumen** from certain crude oils...

# Characterization of natural bitumen Selenizza®SLN

- The analysis of **physico-chemical properties** of natural bitumen Selenizza showed that its **organic phase is similar to** that of petroleum bitumen but having the specificity of **high content of polar fractions** (resin + asphaltene), resulting in a **vitrous transition at higher temperatures**, and in an **enhanced adhesion** between the **bitumen and mineral aggregates**

SARA fractional composition – IATROSCAN method

		Saturated [%]	Aromatic [%]	Resin [%]	Asphaltene-i [%]	I <sub>c</sub>
<b>Purified sample- depth</b>	Average	1,7	24,8	35,1	38,4	0,67
	Standard deviation	0,35	2,29	1,35	1,88	
<b>Purified sample- surface</b>	Average	1,5	22,7	37,2	38,6	0,67
	Standard deviation	0,14	1,37	1,90	1,58	
<b>Raw sample- depth</b>	Average	1,6	23,8	34,6	40,01	0,71
	Standard deviation	0,29	1,40	1,16	1,99	
<b>Raw sample- surface</b>	Average	1,6	19,7	37,9	40,8	0,73
	Standard deviation	0,24	2,02	1,60	2,74	

- The colloidal instability index I<sub>c</sub> values, **indicate** that the organic phases of the asphaltite Selenizza® have a **sol or sol-gel** character, with a sufficient quantity of resins to peptize the asphaltenes

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# Low temperature behaviour

Evolution of the glass transition temperature of the modified bitumen versus the % of Selenizza

	Total heat flux				
	T <sub>g1</sub> [°C]	T <sub>g</sub> [°C]	T <sub>g2</sub> [°C]	ΔT <sub>g</sub> [°C]	ΔΦ [W/g]
<b>Petroleum bitumen 50/70</b>	-31,9	-22,9	-13,2	18,6	0,022
<b>Mixed with 5% Selenizza</b>	-30,9	<b>-23,1</b>	-13,8	17,1	0,019
<b>Mixed with 10% Selenizza</b>	-30,3	-23,1	-13,3	17,0	0,018
<b>Mixed with 15% Selenizza</b>	-32,1	-23,3	-13,4	18,8	0,019
<b>Natural asphaltite Selenizza</b>	-12,6	-1,1	16,2	28,8	0,021

- **Differential scanning calorimetry** showed that the addition of natural bitumen **does not affect** the **glass transition** of bitumen. At the same time it was noted a **slight decrease** of the **crystallizable fraction contents, with the percentage** of the modifier used
- It should be noted that the analysis of mechanical behavior at low temperatures comparing a **35/50 modified bitumen (50/70 + 5% Selenizza)** with a **petroleum bitumen** having the same penetration grade 35/50, showed that the **glass transition temperature** of modified bitumen (typically ranging from -50 to -10°C), was **T<sub>g</sub> = -23.1°C** versus **T<sub>g</sub> = -19.3°C** for the petroleum bitumen, which indicates a **better resistance** of natural bitumen **to brittle fracture**

# Aging effect of natural bitumen

- To evaluate the **aging behavior**, different hard bitumen specimens obtained by modification with natural bitumen, have been submitted to **accelerated aging RTFOT** tests (to simulate oxidation of bitumen during mixture manufacturing) as well as **PAV** (to simulate in-service ageing)
- It was observed that the **aging leads** to bitumen **hardening** which is evidenced by the decrease of penetration and increase softening point temperature TR&B. It is also manifested in an increase of **complex modulus** and **elasticity** (phase angle decrease)



# Selenizza<sup>®</sup>SLN : ageing retarder

## Penetration and TR&B of bitumen before and after ageing

Description	Penetration (dmm)					TR&B (°C)				
	New binder	After RTFOT	$\Delta_1$ (%)	After PAV	$\Delta_2$ (%)	New binder	After RTFOT	$\Delta_1$ (%)	After PAV	$\Delta_2$ (%)
Petroleum 50/70	54	37	31.5	19	64.8	49	53.4	8.9	61.4	25.3
Mixed with 5%	38	27	28.9	15	60.5	52.6	57.2	8.7	66.0	25.4
Mixed with 10%	28	21	25	13	53.5	56.2	60.8	8.1	68.8	22.4
Mixed with 15%	20	14	30	11	45	61.6	65.4	6.1	72.2	17.2
Petroleum 35/50	40	27	32.5	12	70	52.6	56.8	7.9	66.2	25.8
Petroleum 20/30	23	12	47.8	7	69.5	60.0	67.0	11.6	78.8	31.3
Petroleum 10/20	18	9	50	5	72.2	65.0	72.6	11.7	86.0	32.3

**Aging is reflected** in an **increase** of softening point temperature and **decrease** of penetration. These changes ( $\Delta_1$ ,  $\Delta_2$ ) of modified bitumen, are at a **lesser degree compared to the changes** ( $\Delta_1$ ,  $\Delta_2$ ) of petroleum bitumen

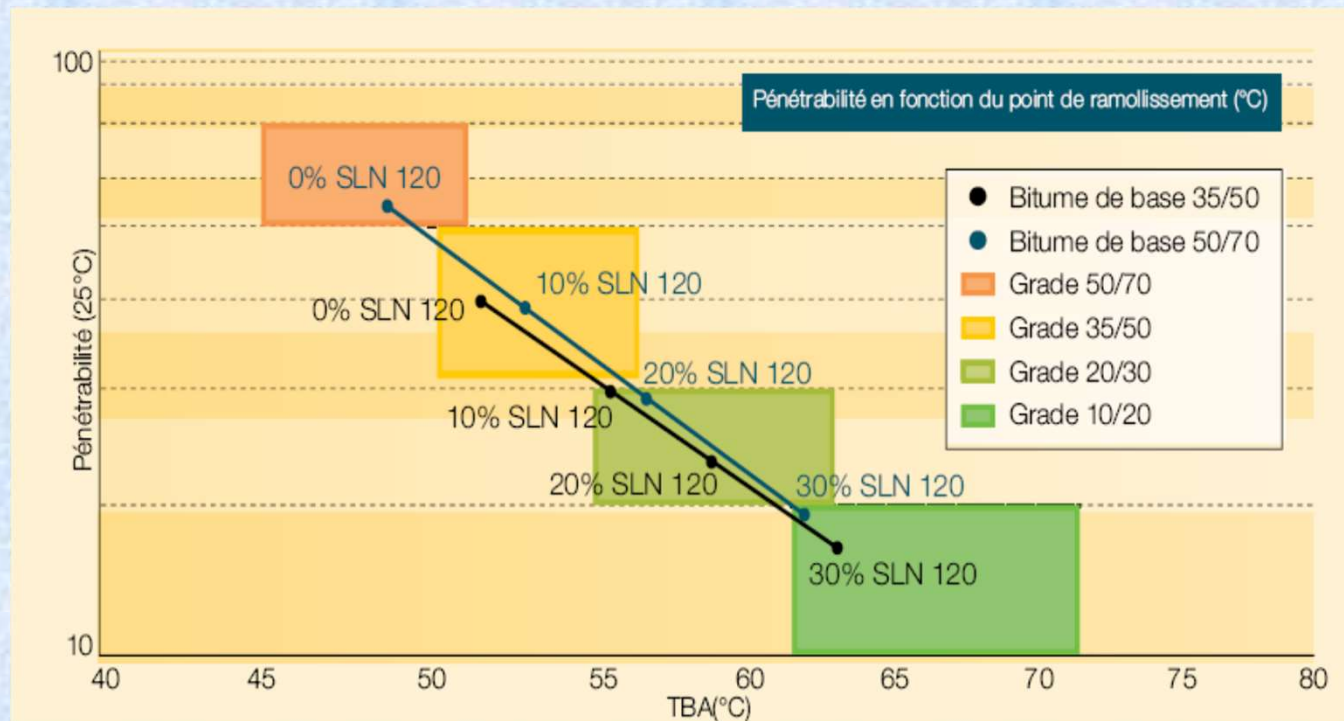
## ***Selenizza: ralentisseur du vieillissement***

- ❖ The **ageing effect** and **thermal fatigue** are coupled. Low temperature fatigue cracking and ageing, **are cumulative** in effect **by amplifying** the **thermal stress** generated during **cooling**. Consequently, it is reasonable to assume that the use of binders **modified with Selenizza**, offers an **advantage** in terms of **behavior** of asphalt mixes **at low temperatures** compared with equivalent petroleum paving grade bitumen



# Total binder modification

- The analysis of **physical-chemical** properties and **mechanical behaviour** of natural bitumen Selenizza, showed that **structurally**, its organic phase **can be compared to petroleum bitumen**, but with **mais** with different proportions of maltenic and asphaltenic fractions, making it **100% compatible with any type of road bitumen**



- Depending on the added quantity of Selenizza and on the base bitumen, it is possible to **obtain precise penetration and/or R&B softening point** value of the resulting binder

# Low-temperature fracture

**EME-01:** with petroleum bitumen 20/30, **EME-02 :** bitumen 50/70 previously modified by SLN, **EME-03:** addition of Selenizza into the mixer

The results presented in the figure show that the **EME-01** is more thermo-rigid compared to the **EME** with natural bitumen

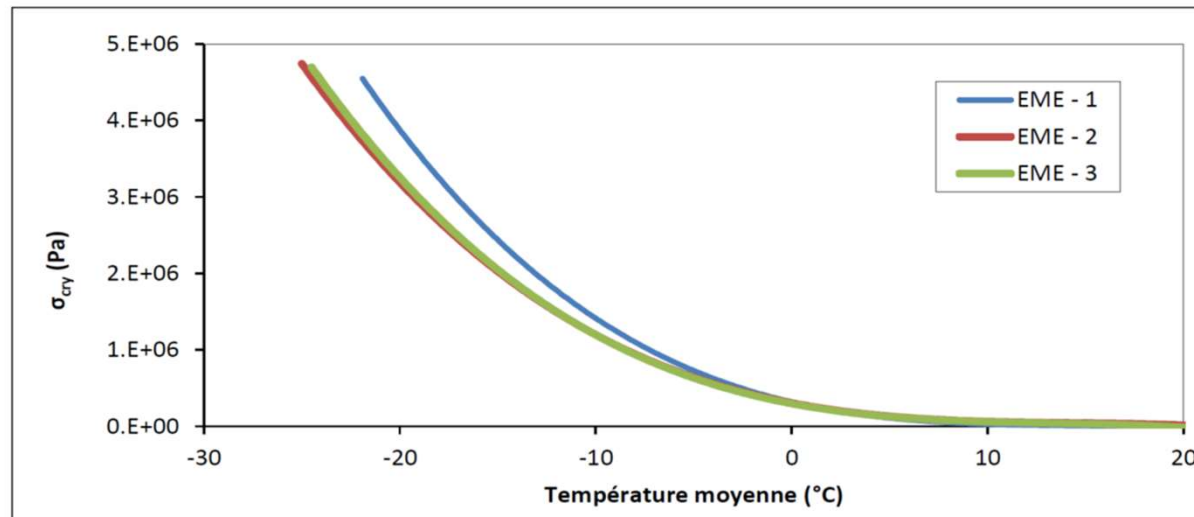


Figure 94 : Contraintes cryogéniques déterminées par l'essai de retrait empêché.



# Low-temperature fracture

The **EME with natural bitumen Selenizza** have better low temperature performance compared to the **EME** manufactured with hard petroleum bitumen of equivalent grade

## Temperatures and thermal stress failure

Référence	$T_{\text{failure}}$ (°C)	Ecart type $T_{\text{failure}}$ (°C)	$\sigma_{\text{cry,failure}}$ (MPa)	Ecart type $\sigma_{\text{cry,failure}}$ (MPa)
<b>EME-01</b>	-21,4	0,27	4,523	-
<b>EME-02</b>	-25,1	0,48	4,752	0,13
<b>EME-03</b>	-24,9	1,47	4,715	0,36

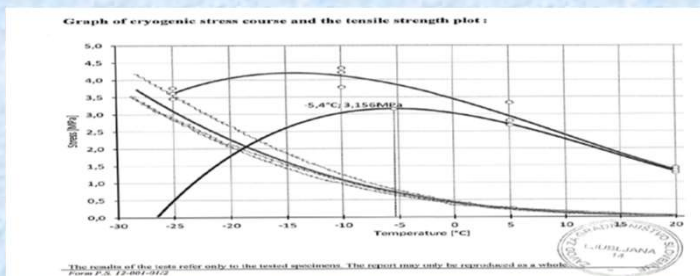
The **EME-02 et EME-03** manufactured with Selenizza are very close to an **EME class 2**, the best performing material according to **European Standards**

# Low-temperature fracture

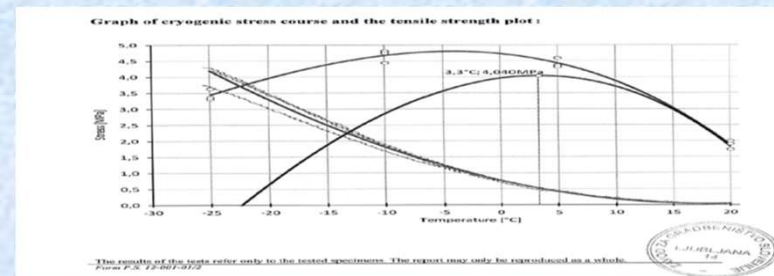
- The Laboratory for Asphalts and Bitumen-Based of the Slovenian National Building Institute (ZAG), conducted TSRST comparative tests on base course asphalt mixture specimen AC 22 with 50/70 pen bitumen, and the same mix design with 50/70 pen bitumen modified with SelenizzaSLN

The tensile strength and cryogenic curves resulting from the tests showed that Selenizza brings **some rigidity** (with Selenizza, the curves are shifted to the right, toward positive temperatures). At **T= 3,3 °C**, the asphalt mixture with Selenizza is subjected to a higher tensile strength **4,04 MPa**, as compared with the tensile strength **3,156 MPa** at **T= - 5,4 °C**, for the classical asphalt mixture

Graph of cryogenic stress course and the tensile strength plot



Binder 50/70



Binder 50/70 + SLN



# Low-temperature fracture

- The TSRST tests show that the addition of Selenizza **has little influence on the low temperature fracture resistance of the asphalt mixture (-25°,3 versus -28°,4 )**

Test results summary :

Failure temperature at TSRST	$T_{\text{failure}}$	-28,4°C
Maximum tensile strength reserve	$\Delta\beta_{t,\text{max}}$	3,156MPa
Temperature at $\Delta\beta_{t,\text{max}}$	$T(\Delta\beta_{t,\text{max}})$	-5,4°C

Binder 50/70

Test results summary :

Failure temperature at TSRST	$T_{\text{failure}}$	-25,3°C
Maximum tensile strength reserve	$\Delta\beta_{t,\text{max}}$	4,040MPa
Temperature at $\Delta\beta_{t,\text{max}}$	$T(\Delta\beta_{t,\text{max}})$	3,3°C

Binder 50/70 + SLN

## Combine the benefits of polymer modified bitumen with the natural bitumen *SelenizzaSLN*

- Generally speaking, studies on petroleum bitumen modified with natural bitumen show that the latter **improve** the behaviour at **high temperatures** (in particular the **rutting resistance**) and **deteriorate** the one at **low temperatures**.
- The **combination** of **natural bitumen** with **polymers** offers an **attractive solution** on a **technical** and on an **economic level**. **A part of SBS** may be **replaced** by natural bitumen in order to **reduce the cost** of asphalt mixture production. Also, according to some authors, the replacement of SBS by natural asphalt, **increases the workability**, which could allow the reduction of the **compaction energy**.



***EME mix design  
examples.  
Selection criteria***

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*Toward High Performance Asphalt Concrete (HPAC) for Cold Climates  
Montreal, September 30, 2016*

# High performing EME (Switzerland)

In order to respond to the **technical challenges** imposed by:

1. very **severe stresses** and strains that bituminous pavements are subject to due to the **large increase** in the number of **lorries** crossing the Swiss Alps every year
2. **very harsh climatic** conditions of the country  
(temperatures fluctuate between  $-20^{\circ}\text{C}$  and  $+40^{\circ}\text{C}$ )

Switzerland has integrated in its national standard for bituminous mixtures, the **concept of High Modulus Asphalt Mixes (EME)**

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# High performing EME (Switzerland)

- **The performance class 1** is recommended to improve the **resistance to permanent deformation** (rutting)
- **The class 2**, to improve the **fatigue resistance** of the asphalt mix layer. More difficult to reach, it includes **tough requirements** on **stiffness modulus** and **fatigue resistance** (more severe than the French one) :

## *Specifications of Swiss standard on EME*

	Méthode d'essai	AC EME 22 C1	AC EME 22 C2
Teneur en vides des éprouvettes Marshall (%)	EN 12697-8	≤ 3.0 - 5.0	≤ 1.0 - 3.0
Sensibilité à l'eau, résistance à la traction par fendage ITSr (%)	EN 12697-12	≥ 70	≥ 70
Teneur en liant en pourcentage de la masse d'enrobé (%)		≥ 4.6	≥ 5.4
Résistance à l'orniérage à 30 000 cycles et 60 °C	EN 12697-22		
Profondeur d'ornière sur une plaque de 10 cm d'épaisseur (%)		≤ 5.0	≤ 7.5
Module complexe à 15 °C/10 Hz (MPa)	EN 12697-26	≥ 11 000	≥ 14 000
Résistance à la fatigue à 10 °C/25 Hz (microdéformations)	EN 12697-24	≥ 100	≥ 135

Tableau 1  
Spécifications de la norme suisse SN 640 431-1NAB pour les AC EME 22

# High performing EME (Switzerland)

- To respond to this constraints, **CO.MI.BIT**, an **asphalt mix manufacturing cooperative**, located in Tavernes (Canton Ticino), has developed a new mix design of type **AC EME 22 C2** that improves the **fatigue performance** by using a **polymer modified bitumen** all while maintaining a high stiffness modulus using **Selenizza®SLN** as hardening additive. In the specific case, the binder was composed of a Shell Cariphalte 25 RC polymer modified bitumen and natural bitumen Selenizza SLN
- Based on the **same grading curve**, two alternatives of mix design have been tested containing different dosage levels of Selenizza, to determine its percentage for obtaining a final binder with penetration ranging between **10 to 20 dmm**



# High performing EME (Switzerland)

1. First formulation (Selenizza **26%** of the total binder):

**3.9%** Shell Cariphalte 25 RC+ **1.4%** SLN = **5.3%**

2. Second formulation (Selenizza **29%** of the total binder):

**3.9%** Shell Cariphalte 25 RC+ **1.6%** SLN = **5.5%**

Composition du liant	Unité	Formule 1	Formule 2
Shell Cariphalte 25 RC	%	3,9	3,9
SLN 120	%	1,4	1,6
Teneur en liant théorique (en % de la masse d'enrobé)	%	5,3	5,5
Module complexe à 15 °C/10 Hz (EN 12697-26)	MPa	19 441	18 336
Pourcentage de vides hydrostatique	%		
Résistance à la fatigue à 10 °C/25 Hz (EN 12697-24)	Microdef	139	145
Pourcentage de vides hydrostatique	%		

Tableau 4

Résultats des essais de module et de fatigue obtenus par Shell Global Solutions

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# High performing EME (Switzerland)

- The obtained **modulus** and **fatigue** tests results **clearly exceed** the Swiss standard specification for the asphalt mixes AC EME 22 C2
- **The addition of 29%** Selenizza gives poorer results. An explanation of this could be that beyond a certain proportion of Selenizza, **the assimilation becomes more difficult** and would not contribute to increasing the asphalt mix performances
- To prevent the **cracking risk** at low temperatures, **a new job** mix formula was envisioned and then verified by **LAVOC Laboratory** at the Swiss Federal Institute of Technology Lausanne



# High performing EME (Switzerland)

- The mix design was modified with a **less strong value** of the **stiffness modulus** by introducing a lower percentage of Selenizza (**22%**), while maintaining a **high level of fatigue resistance**, :

**4.7% Shell Cariphalte 25 RC+ 1.4% SLN = 6.1%**

Richness modulus **K= 3.74**

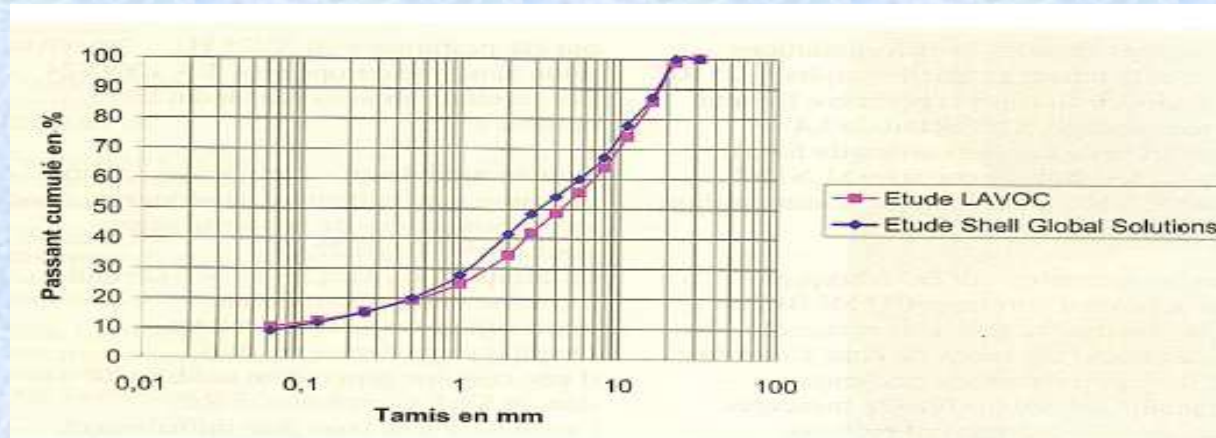


Figure 1  
Courbes granulométriques des enrobés AC EME 22 testés

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# High performing EME (Switzerland)

The tests performed on **extracted binder**, indicated that it belonged to a **10/20** paving grade bitumen:

- ❑ **penetration = 13 dmm**
- ❑ **TR&B = 86,7°C**

Test results conducted by LAVOC, was the following (**void content= 2.4%**):

- ❑  **$\epsilon_6$  (extrapoled)  $\approx$  150  $\mu$ def** (Swiss standard  $\geq 135$   $\mu$ def)
- ❑ **Modulus (15°C/10 Hz) = 15 100 MPa** (Swiss standard  $\geq 14$  000 MPa)



# High performing EME (Switzerland)

- Other mix design of type **AC EME 22 C1** were developed and validated in cooperation with **LAVOC Laboratory** at the Swiss Federal Institute of Technology Lausanne, with very good results in terms of fatigue performance and with low susceptibility to rutting

**3.9 % PmB Shell Cariphalte 25 RC + 1,4% SLN = 5.3%**

## ***Test results:***

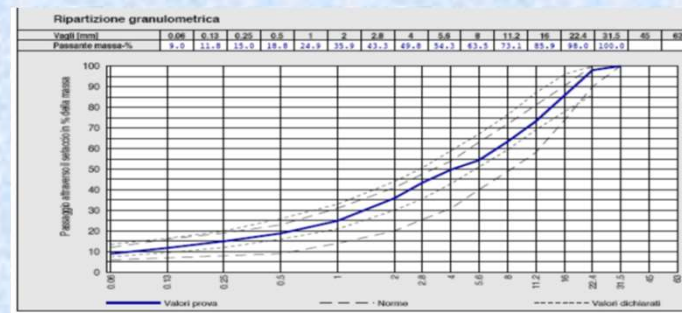
- Richness modulus  $K=3.30$**  (standard  $\geq 2.7$ )
  - Rutting (at 30 000 cycles) = 1.9 %** (standard  $\leq 5\%$ )
  - $\epsilon_6$  (extrapolated)  $\approx 134$  microdéformations** (standard  $\geq 100 \mu\text{def}$ )
  - Modulus (15°C/10 Hz) = 18 016 MPa** (standard  $\geq 11\ 000$  MPa)
- The **high value of richness modulus** generates good **fatigue performances** and the asphalt mix has **low rutting susceptibility**

# High performing EME (Switzerland)

- It should also be noted the use of Selenizza with the recycled aggregates

Example: **AC EME 22 C2** with binder Shell B 15/20 + 10% RA + 0.3% SLN

Binder content = **5.34%** (4.4% Shell 15/20 + 0.64%RA + 0.3% SLN)



- Rutting** (at 30 000 cycles) = **3.8 %** (standard  $\leq 7.5\%$ )
- $\epsilon_6$  (extrapolated)  $\approx$  **153** microdéformations (standard  $\geq 130 \mu\text{def}$ )
- Modulus** (15°C/10 Hz) = **14 800 MPa** (standard  $\geq 14\ 000 \text{ Mpa}$ )

- The mixture has low rutting susceptibility **and is effective in terms of fatigue resistance**. The good behavior that was observed was also due to the addition of Selenizza

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# High performing EME (Switzerland)

- In Switzerland, after 10 years' **service with harsh winters**, in the various road construction projects where Selenizza was used for the manufacture of high performing EME , **no thermal cracks were found** confirming the relevance of these EME mix designs that have led to **high mechanical performances**
- These results **confirm the potential** for successfully **combining** the benefits of **polymer modified bitumen** and of natural bitumen **Selenizza SLN**



# Construction sites with Selenizza®SLN



2011 : Bridge Val Verzaska, Ticino - Switzerland

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# Construction sites with Selenizza®SLN



Lugano - Switzerland

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# Construction sites with Selenizza®SLN



Mastic asphalt Switzerland

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# Construction sites with Selenizza®SLN



Highway Ticino - Switzerland

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# Construction sites with Selenizza®SLN



2011 : highway bypass Bern -Switzerland

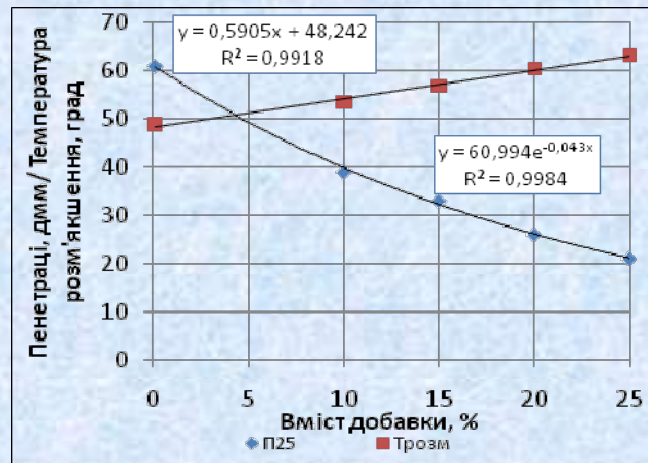
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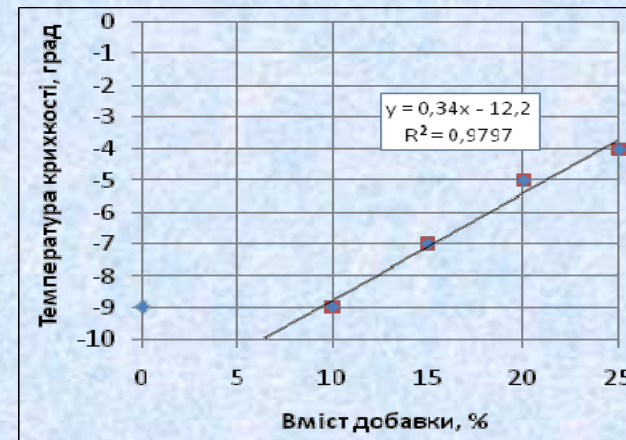


# High performing asphalt mixes in Ukraine

In Ukraine, SelenizzaSLN was **legalized as construction material**. It has been classified as a bitumen modifier for asphalt mixes that should be inserted to a proportion of **4-12% by mass of the base bitumen**. **The National Technical University of Ukraine** has analyzed the properties of Selenizza aiming to determine its compatibility with the Ukrainian bitumen (**60/90 grade bitumen**) and with those of **bordering foreign countries**.



*TR&B and Penetration Modification of BND 60/90 bitumen with the % of Selenizza*



*Fracture Temperature Modification of BND 60/90 with the % of Selenizza*

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# High performing asphalt mixes in Ukraine

The analysis showed that the addition of Selenizza up to **10%**, **does not affect the Fraas temperature of 60/90 bitumen**. Above this %, a **proportional increase** of the Fraas point with the % of Selenizza was observed

SLN [%]	0	10	15	20	25
Fraas T [°C]	-9	-9	-7	-5	-4

**In general, the percentage of SelenizzaSLN used in Ukraine varied from 4% to 16% (mainly 5% and 8%), in different heavy traffic areas operating under harsh climatic conditions with temperatures fluctuating between -30 to + 30°C**

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# High performing asphalt mixes in Ukraine

- Highway **Kiev – Kovel**, in the **western part of Ukraine**, surface paving SMA -20, 8cm base course & 8cm binder course, on 3 segments with a total length of approximately **5 km**



with Selenizza



with SBS

*After 3 years' service, the road is still in a very good condition !!!*

In the middle of the highway constructed using Selenizza, on a small section, **for comparison purposes**, was used a **Kraton modified binder**. The asphalt roadway surface with Selenizza is **smoother** and is more **black in color** compared to the segment where Kraton modified binder was used

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# High performing asphalt mixes in Ukraine

Zhitomir, 70 Km west of Kiev



*Before*



*After*

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# High performing asphalt mixes in Ukraine



National highway Mykolaiv (Ukraine)

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# High performing asphalt mixes in Ukraine

## Kiev



SMA with 6 % Selenizza



Heavy traffic highway interchange entering Kiev

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# High performing asphalt mixes in Ukraine



Ring road around Kiev (Ukraine)

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# High performing asphalt mixes in Ukraine

**Helicopter landing** pad in the downtown Kiev near Parliament building, constructed with asphalt mix using **6,5% Selenizza**



After **5 years' service**, it resulted that the use of SelenizzaSLN was very effective, in general there were no evidence of rutting or other **FRAAS breaking** point related **damages**. The resistance to **permanent deformation** increased by a factor of **1,5**

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# An environmentally friendly bitumen | 4

*Toward High Performance Asphalt Concrete (HPAC) for Cold Climates  
Montreal, September 30, 2016*

# LIFE CYCLE ASSESSMENT

## SELENIZZA compared to petroleum bitumen

- Worldwide economic crisis and environmental awareness have created the need for **bituminous binders** that meet **Life Cycle Assessment constraints**.
- Life Cycle Assessment (LCA) assess the durability of de differents materials evaluating the environmental impact during all the stages of the product's life cycle, from cradle to grave
- More and more we need to **quantify** the **environmental impact** of construction materials and compare **potential solutions** based on **scientific data**



# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

As a part of a common commitment to **sustainable development**, the **University of Rome** in cooperation with the company **Selenice Bitumi**, carried out a **research project**, whose aim was to **analyze and compare** for the first time, in terms of **energy consumption** and **CO<sub>2</sub> emission** between:

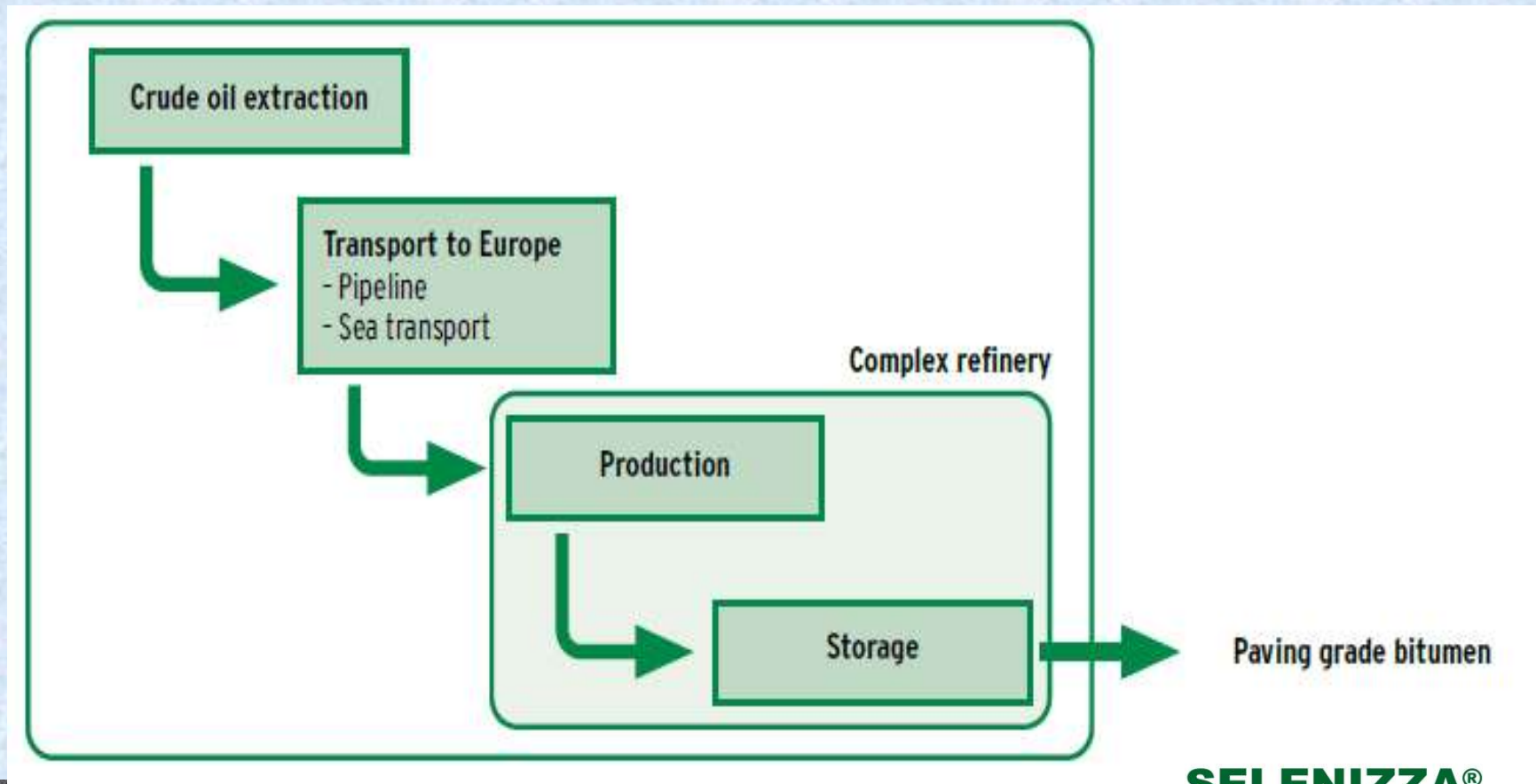
1. the various steps necessary to produce the **conventional bitumen from crude oil**
2. the production process of the **Albanian natural asphalt** (Selenizza)

The logo for Selenizza Natural Bitumen, featuring the brand name in green and the product type in white on a green background.

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# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

*Petroleum bitumen production chain (cradle to grave approach)*



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# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

- The study was carried out **in accordance** with the guidelines of **EU regulations** (ISO 1440 and 14044) for environmental assessment, called LCA (Life Cycle Assessment) and LCI (Life Cycle Inventory), and **data have become available** from **relevant bodies** and specialized agencies such as for example, Eurobitume & EAPA (European Asphalt Pavement Association)
- The **Life Cycle Inventory (LCI)** for **straight-run bitumen**, has evaluated all the **ressources & inputs** (raw materials, electricity, fuel, etc.)

# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

## Consommation d'énergie et émission CO<sub>2</sub> pour les bitumes routiers de distillation

Production 1 tonne bitume (processus avec infrastructure)	unité	Extraction pétrole brut	Transport	Raffinage	Stockage	Total
<i>Matière première</i>						
Pétrole brut	kg	1000				1000
<i>Consommation de ressources énergétiques</i>						
Gaz naturel	MJ/t	2,196		0,855	0,001	3,061
Pétrole brut	MJ/t		0,588	0,404	0,096	1,088
Electricité	MJ/t					0,561
Total	MJ/t					4,71
<i>Emissions dans l'air</i>						
CO <sub>2</sub>	g	144563	37422	7831		226167





# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

## *Deposit of natural bitumen Selenizza*



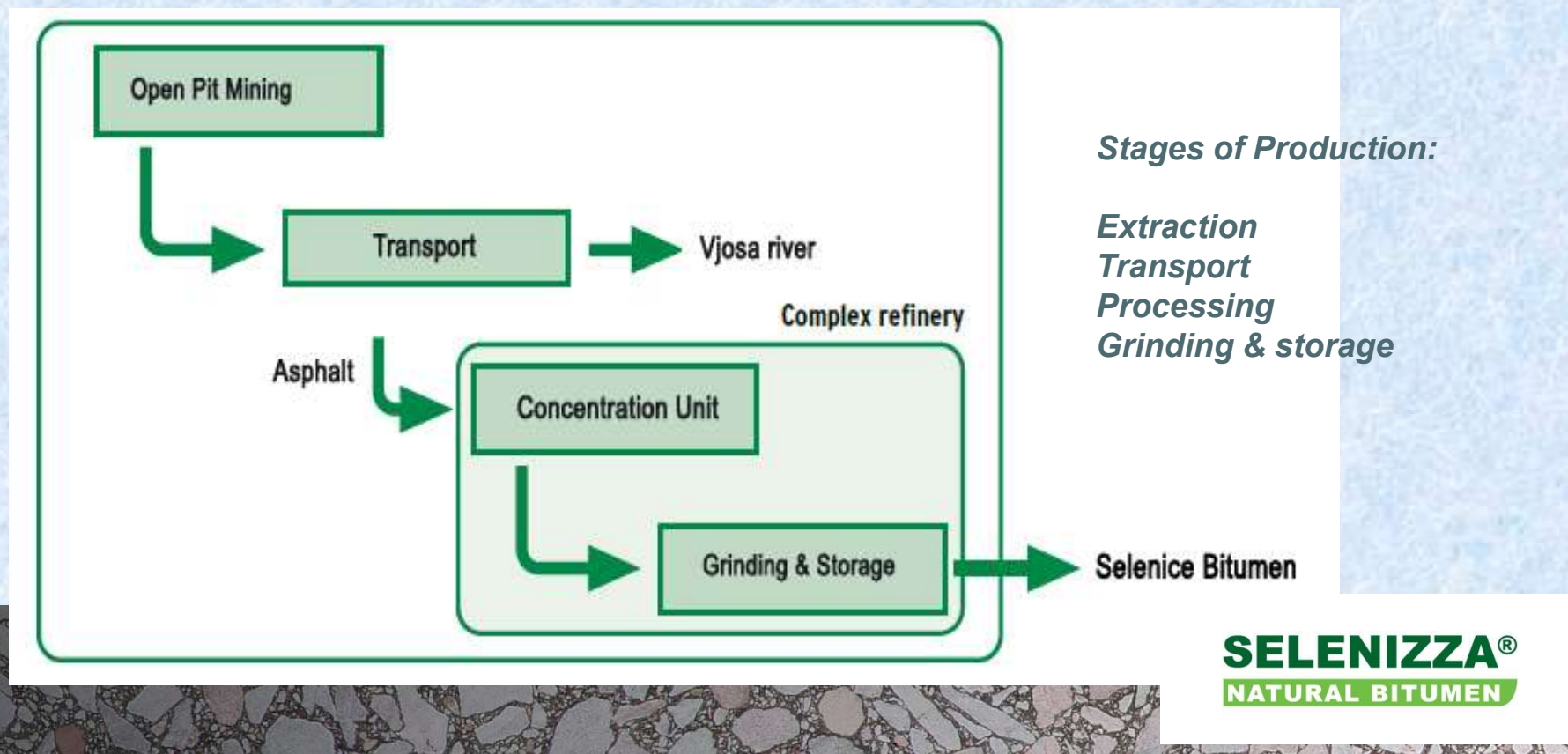
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# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

## *The production chain of natural bitumen Selenizza*

*The production process is **far simpler** with a direct impact on the **energy saving**; also the **transport cost is reduced** to minimum because the **processing unit** is located **close to the deposit***





# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

- The mine of Selenice manufactures on site:
  - the **raw ore** (natural bitumen)
  - **The fuel** (bituminous coal) used for the processing of the raw ore in the heaters
  - **The residual inorganic materials are** transported and deposited close to a river in the vicinity
- In order to assess the energy consumption, has been used all the **technical documentation** of electrical equipments and mine vehicles. The **value Italo-Albanian** energy mix, has been obtained from the International Energy Agency **IEA**
- The **calorific value of the fuels**, and thus the amount of **CO<sub>2</sub> emissions per kg** of fuel burned, were obtained from **ENI** (Italian State Hydrocarbons Authority) data base

# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen


## Consommation d'énergie et émission CO<sub>2</sub> pour l'asphalte naturel Selenizza

Production 1 tonne bitume (processus avec infrastructure)	unité	Extraction asphalte brut	Transport	Unité de Traitement	Stockage	Total
<i>Matière première</i>						
Asphalte brut	kg	1000				1000
<i>Consommation de ressources énergétiques</i>						
Essence	MJ/t	1,007				1,007
Diesel	MJ/t		0,066		0,001	0,067
Charbon bitumineux	MJ/t			0,339		0,339
Electricité	MJ/t					0,963
<b>Total</b>	<b>MJ/t</b>					<b>2,376</b>
<i>Emissions dans l'air</i>						
CO <sub>2</sub>	g	59300	4500	59145		<b>127298</b>



# LIFE CYCLE ASSESSMENT SELENIZZA compared to petroleum bitumen

## *Comparing the results*



Bitumes routiers de distillation						
Total	Consommation d'énergie	MJ/t				4,71
CO <sub>2</sub>	Emissions dans l'air	g	144563	37422	7831	226167

L'asphalte naturel Selenizza						
Total	Consommation d'énergie	MJ/t				2,376
CO <sub>2</sub>	Emissions dans l'air	g	59300	4500	59145	127298

- **Selenizza's** production cycle has an **environmental impact** approximately **44% less** than the distillation bitumen
- **Energy consumption** is also reduced by **around 50%** compared to bitumen produced from crude oil

# ***Conclusions***

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*Toward High Performance Asphalt Concrete (HPAC) for Cold Climates  
Montreal, September 30, 2016*



# Conclusions

- **100% compatible** with bitumen from refinery (and polymer modified bitumen)
- High performance **in modulus & permanent deformation**
- Better **bitumen-aggregates adhesion**
- Pavement **thickness reduction**
- Better **workability**
- **Aging retarder & Higher lifetime** of the pavements
- **Minor environmental impact**



***Thank you for your attention!***

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